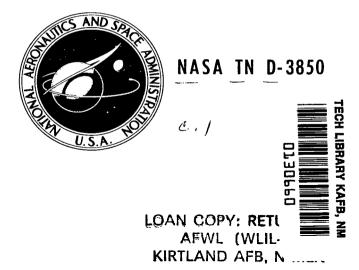
NASA TECHNICAL NOTE



PREDICTIONS OF SHOCK-LAYER RADIATION FROM MOLECULAR BAND SYSTEMS IN PROPOSED PLANETARY ATMOSPHERES

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SUMMARY

Concentrations of radiating molecules and radiation from a number of band systems are presented for equilibrium shock-layer temperatures and densities of vehicles entering proposed Martian and Venusian atmospheres. The atmospheres selected consist of various proportions of $\rm CO_2$, $\rm N_2$, and A. Charts are also presented which relate these equilibrium shock-layer properties to flight velocity and ambient density through the normal shock conservation equations. These data can be used to estimate stagnation-point radiative heat transfer for entry trajectories. Estimates for a few selected flight conditions are discussed and compared.

INTRODUCTION

There is increasing interest in the radiative heating of vehicles entering the atmospheres of Mars and Venus. One constituent of these atmospheres, CO_2 , has been identified, but its abundance, as well as the nature and abundance of other gases, is still uncertain. In addition to CO_2 , proposed atmospheres usually consist of various proportions of N_2 and A (refs. 1-5).

Seven mixtures intended to cover the range of uncertainty in these proportions are considered in the present report. The first four include a more likely range for the Martian atmosphere, since latest evidence indicates that CO₂ is at least a major constituent (ref. 4). The mole fraction composition of the seven mixtures considered in the present study is given in the following table:

<u> </u>	N ₂	_A
0.50	0.50	0
•50	•30	.20
•50	0	•50
1.00	0	0
0	1.00	0
. 25	•75	0
•75	. 25	0

To include a range of possible shock-layer conditions caused by uncertainties in the density of the Martian and Venusian atmospheres, temperatures from 4,000° to 12,000° K and density ratios from 10°5 to 1 are considered for each mixture. The radiative intensity for 10 of the more well-known band systems considered to be major radiative contributors and the concentration of radiating molecules were then calculated for these conditions. Normal shock properties were also calculated to relate these shock-layer properties to flight conditions. The assistance of Dr. Victor H. Reis in calculating the effects of self-absorption for the CN violet band system is gratefully acknowledged.

SYMBOLS

Вe	rotational constant, cm ⁻¹
$\mathbb{B}_{\mathbf{V}}$	rotational parameter that varies with vibrational level, cm-1
\mathtt{B}_{λ}	Planck black-body function, $\text{W/cm}^2\text{-sr-}\mu$
С	velocity of light, cm/sec
$\mathbf{E}_{\mathbf{V}}$	vibrational energy, cm ⁻¹
$\mathbf{E}_{3}(\tau)$	function of τ used in self-absorption expression (eq. (12))
е	electronic charge, esu
Fel,T	fractional population of the electronic state
f ^{abs} e l	electronic absorption oscillator strength for the band system (f number)
h	Planck constant, erg-sec
I	total intensity, W/cm3
	total intensity, with
I_p	total intensity per particle, W/particle
\mathbf{I}_{p} $\mathbf{I}_{\mathrm{p}_{\lambda}}$	
	total intensity per particle, W/particle
$\mathbf{I}_{\mathbf{p}_{\lambda}}$	total intensity per particle, W/particle spectral intensity per particle, W/ μ particle
$\mathbf{I}_{\mathbf{p}_{\lambda}}$ \mathbf{I}_{λ}	total intensity per particle, W/particle spectral intensity per particle, W/ μ particle spectral intensity, W/cm³- μ
$I_{p_{\lambda}}$ I_{λ} K_{λ}	total intensity per particle, W/particle spectral intensity per particle, W/ μ particle spectral intensity, W/cm ³ - μ spectral absorption coefficient, cm ⁻¹

```
Q_{\mathbf{v}}
           vibrational partition function
           Franck-Condon factor
qv tv"
           total heating rate, W/cm<sup>2</sup>
ģ
\dot{	extbf{q}}_{\lambda}
           spectral heating rate, W/cm^2-\mu
R
           ratio of total self-absorbed heating rate to optically thin rate
           temperature, <sup>O</sup>K
\mathbf{T}
Тe
           electronic energy, cm-1
V
           flight velocity, km/sec
v
           vibrational quantum number
           maximum vibrational quantum number (eqs. (6) and (7))
           vibration-rotation interaction constant, cm<sup>-1</sup>
\alpha_{\mathsf{e}}
δ
           shock standoff distance, cm
λ
           wavelength, µ
           wave number, cm<sup>-1</sup>
           band-head wave number, cm-1
           density, g/cm<sup>3</sup>
ρ
           density of air at 1 atm and 273^{\circ} K, 1.293 \times 10^{-3} g/cm<sup>3</sup>
ρ
           vibrational constants, cm<sup>-1</sup>
                                           Subscripts
OT
           optically thin
SA
           self-absorbed
           conditions ahead of shock wave
1
2
           conditions behind shock wave
```

Superscripts

- (') upper electronic state
- (") lower electronic state

CALCULATIONS

Computer programs developed at Ames Research Center (ref. 6) were used to calculate the concentrations of radiating molecules and other equilibrium thermodynamic shock-layer properties for atmospheres, temperatures, and densities of interest. These properties were then related to flight velocity and ambient density by solving the normal shock conservation equations. Number densities of radiating molecules are given in tables I through VII, and temperatures and densities behind normal shock waves are plotted in figures 1 to 7 for an ambient temperature of 300° K.

Calculations of the spectral intensities of the CN violet, CN red, CO fourth positive, C_2 swan, NO beta, NO gamma, N_2 first positive, N_2 second positive, N_2^+ first negative, and O_2 Schumann-Runge band systems used the "smeared line" model given by Williams and Treanor (ref. 8). The fundamental assumption of this model is that the density of rotational lines is so great that the distribution of their intensities may be regarded as continuous. This model gives a reasonably accurate representation of the gross features of band systems; other examples of its use are given in references 9 and 10.

From equation (7) of reference 8, the spectral intensity is

$$I_{\lambda} = 1.19 \times 10^{-16} \frac{\pi e^{2}}{mc^{2}} \frac{n_{p} f_{el}^{abs} F_{el,T}^{"} B_{e}^{"}}{k \nu_{oo}^{o} T Q_{v}^{"}} \frac{\nu^{e}}{e^{\nu/kT} - 1} \sum_{q_{v} f_{v}^{"}} \frac{q_{v} f_{v}^{"}}{|B_{e}^{"} - B_{e}^{"}|} e^{-\frac{B_{e}^{"}}{|B_{e}^{"} - B_{e}^{"}|} (\nu - \nu_{v}^{o} f_{v}^{"}) + E_{v}^{"}}{kT}, \quad \text{W/cm}^{3} - \mu - \text{sr}$$

$$(1)$$

where the summation is such that $v_{V^!V^"}^O \leq \nu$ for bands degraded to shorter wavelengths and $v_{V^!V^"}^O \geq \nu$ for bands degraded to longer wavelengths. Williams and Treanor (ref. 8) stated that it was more exact to use B_V in place of B_e in that part of equation (1) included in the summation, where

$$B_{V} = B_{e} - \alpha_{e} \left(v + \frac{1}{2} \right), \quad em^{-1}$$
 (2)

¹The CN radical is an important radiator, but the correct values of calculated CN concentrations are uncertain, primarily because of the wide range of values of heat of dissociation reported in the literature (from 7.5 to 8.5 eV), none of which is clearly better than any other (ref. 7). The value used here is approximately 8.2 eV.

They also indicated later in a private communication that the induced emission factor $1-e^{-hc\,\nu/kT}$, as well as the factor hc, had been inadvertently omitted. After these corrections and modifications are made, the expression is multiplied by $^4\pi$ to obtain the radiation in all directions ($^4\pi$ sr) and divided by $n_D.$ The equation, as evaluated in this report, then becomes

$$I_{p_{\lambda}} = 1.9 \times 10^{-27} \frac{f_{el}^{abs} F_{el,T}^{"} B_{e}^{"}}{v_{oo}^{O} T Q_{v}^{"}} v^{s} e^{-\frac{hc v}{kT}} \sum_{|B_{v}^{l} - B_{v}^{"}|} \frac{q_{v} v_{v}^{"}}{|B_{v}^{l} - B_{v}^{"}|} e^{-\frac{hc v}{B_{v}^{l} - B_{v}^{"}}} (v - v_{v}^{O} v_{v}^{"}) + E_{v}^{"}}{|B_{v}^{l} - B_{v}^{"}|}, \quad \text{W/μ particle}$$
(3)

where

$$E_{v} = \omega_{e}\left(v + \frac{1}{2}\right) - \omega_{e}x_{e}\left(v + \frac{1}{2}\right)^{2} + \omega_{e}y_{e}\left(v + \frac{1}{2}\right)^{3} - \omega_{e}z_{e}\left(v + \frac{1}{2}\right)^{4}$$
, cm^{-1} (4)

$$Q_{\mathbf{v}}^{\mathbf{n}} = \sum_{\mathbf{v}^{\mathbf{n}} = \mathbf{0}}^{\mathbf{v}_{\mathbf{M}}^{\mathbf{n}}} e^{-\operatorname{hc} \mathbf{E}_{\mathbf{v}}^{\mathbf{n}}}$$

$$(6)$$

and $v_{M}^{"}$ is the smallest value for which

$$\frac{\frac{-\operatorname{hcE}_{\mathbf{v}}^{\mathbf{n}}}{\operatorname{kT}}}{\frac{\operatorname{vM}_{\mathbf{M}}^{\mathbf{n}}}{\sum_{\mathbf{v}}^{\mathbf{n}} = 0}} \stackrel{-\operatorname{hcE}_{\mathbf{v}}^{\mathbf{n}}}{\operatorname{e}^{-\operatorname{kT}}} \leq 0.001 \tag{7}$$

The values of T_e , B_e , ω_e , $\omega_e x_e$, $\omega_e y_e$, $\omega_e z_e$, and α_e were taken from Herzberg (ref. 11); the fraction of molecules in the lower electronic state, $F_{e\,l,T}^{"}$, was computed by formulas obtained from Gilmore (ref. 12), and the vibrational quantum numbers for the band-head transitions considered were those listed by Wallace (refs. 13, 14). The values and sources of the band-system electronic-absorption oscillator strengths (f numbers) used, and the sources of the Franck-Condon factors are given in table VIII. Thus, the spectral intensity per particle, $I_{p_{\lambda}}$, of each band system was calculated from equation (3) and plotted for five temperatures in figures 8 to 17. The total intensity per particle, $I_{p_{\lambda}}$, of each band system was obtained by integrating the spectral

intensity with respect to wavelength over the spectral range of the band system. Values of $\rm I_p$ and the spectral ranges used in the calculations are listed in table $\rm IX.^2$

DISCUSSION

These tables and graphs can be used to estimate stagnation-point radiative heating along proposed planetary entry trajectories. The procedure will be described and sample calculations of radiative heating at two points of a proposed trajectory through the first five atmospheres in the table on page 1 will be discussed and compared.

The temperature and density behind a normal shock wave can be determined from figures 1 to 7 as a function of flight velocity and ambient density for a particular atmosphere, and should be only slightly affected by ambient temperatures different from 300° K. These shock-layer conditions are then used to interpolate for $\rm n_p$, the concentration of molecules, in tables I to VII. Interpolation in figures 8 to 17 or table IX using the shock-layer temperature gives $\rm I_p$ and $\rm I_p$, respectively. The spectral intensity of each band system is then

$$I_{\lambda} = n_p I_{p_{\lambda}}$$
, $W/cm^3 - \mu$ (8)

Similarly, the total intensity of each band system is

$$I = n_p I_p , \quad W/cm^3$$
 (9)

At the stagnation point of a blunt body, the spectral radiative heating rate for an optically thin gas in thermochemical equilibrium is given by the plane-layer approximation (ref. 15) as

$$\dot{q}_{\lambda_{\rm OT}} \approx \sum \frac{I_{\lambda} \delta}{2}$$
, $W/cm^2 - \mu$ (10)

and, similarly, the total rate is

$$\dot{q}_{OT} \approx \sum_{18} \frac{18}{2}$$
, W/cm² (11)

where the summation includes all band systems and $\,\delta\,$ is the shock-wave standoff distance.

 $^{^2\}mathrm{Since}$ the f number is considered constant over the entire band system in the method expressed by equation (3), the effect of a better f number on the given values of I_{p_λ} and I_p can be obtained by simply multiplying the given values by the ratio of the new f number to the given f number.

At the first point of an example trajectory, $V_1 = 6.5 \text{ km/sec}$ and ρ_1/ρ_0 = 10⁻⁴. In an atmosphere of 50 percent CO₂ and 50 percent N₂, T₂ = 5600⁰ K and ρ_2/ρ_0 = 1.775×10⁻³. Figure 18 is a plot of equation (8) for these conditions showing the spectral distribution and intensity of the band systems. The total heating rate, obtained by evaluating equation (11), is shown in figure 19. In 50 percent CO2 and 50 percent N2, most of the radiation comes from the CN(V), CN(R), and CO(4+) band systems; other contributions are smaller by factors of 100 to 1000. In 50 percent CO2, 30 percent N2, and 20 percent A, the shock-layer temperature is about 2000 higher (5830° K) , and the total radiation is somewhat higher. In 50 percent CO_2 and 50 percent A, the only contributions come from CO(4+), $C_2(S)$, and $O_2(S-R)$, but the latter two band systems are still negligible compared to CO(4+). Moreover, although the shock-layer temperature is about 600° higher (6450° K), the absence of CN(V) and CN(R) results in reduced total radiation. In 100 percent CO₂, the shock-layer temperature is about 800° lower (5650° K), and the total radiation, which again is from the CO(4+), $C_2(S)$, and $O_2(S-R)$ systems, is the lowest of the four gas mixtures considered thus far, but still more than 1/3 that from the highest. In 100 percent N_2 , the shock-layer temperature is about 2000 higher (58700 K), but the only contributions come from $N_2(1+)$, $N_2(2+)$, and $N_2^+(1-)$. The total radiation in this case is about a factor of 100 lower than that from any of the previous four gas mixtures.

At the second point of the proposed trajectory, V_1 = 5.8 km/sec and ρ_1/ρ_0 = 10⁻³. The total radiation from the first three gas mixtures and 100 percent N_2 is about a factor of 10 higher than at the previous trajectory point. In 100 percent CO_2 , however, the total radiation is about a factor of 10 lower, mainly because of a shock-layer temperature which is about 12000 lower (44000 K) than at the previous point.

Experimental evidence supporting similar predictions is discussed in reference 16. It should be noted that there are other sources of radiation, such as continua and atomic lines, that contribute importantly at high temperatures. In fact, continuum and line radiation are expected to be dominant above about $11,000^{\circ}$ K (ref. 16).

An expression that accounts for self-absorption and is shown to be a good approximation for the stagnation-point radiative heating of a blunt body is given by Kennet and Strack (ref. 17) and Strack (ref. 18).

$$\dot{q}_{\lambda_{\rm SA}} \approx \pi B_{\lambda} [1 - 2E_3(\tau)]$$
, $W/cm^2 - \mu$ (12)

where B_{λ} is the Planck black-body function, values of $E_3(\tau)$ tabulated by Kourganoff (ref. 19) are plotted in figure 20 as a function of τ , and

$$\tau = K_{\lambda} \delta \tag{13}$$

where

$$K_{\lambda} = \frac{I_{\lambda}}{4\pi B_{\lambda}}$$
, cm^{-1} (14)

is the spectral absorption coefficient. Hence, if differences between values from equations (10) and (12) are appreciable in a particular spectral region, the more realistic value of \dot{q}_{SA} can be obtained by replacing the optically thin contribution indicated in equation (11) by the integral of equation (12) in this region. This procedure shows that radiation from the CN(V) and the CO(4+) band systems can be reduced by self-absorption. The ratio

$$R = \frac{\int_{0}^{\infty} \dot{q}_{\lambda_{SA}} d\lambda}{\int_{0}^{\infty} \dot{q}_{\lambda_{OT}} d\lambda} = \frac{\dot{q}_{SA}}{\dot{q}_{OT}}$$
(15)

for these systems is plotted as a function of temperature and density in figures 21 and 22 for a mixture of 50 percent $\rm CO_2$ and 50 percent $\rm N_2$, and shock-wave standoff distances of 1 and 20 cm. At higher shock-layer densities, most of the radiation is self-absorbed.

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TABLE I.- NUMBER DENSITY, MOLECULES/CM3: 50 PERCENT CO2 - 50 PERCENT N2

T2, OK	log ₁₀ ρ ₂ /ρ ₀	N2	N ₂	co	02	C2	CN	NO
4,000	-5	9.629 +13	7.304 +5	1.079 +14	2.791 +9	9.651 +5	3.178 +10	1.543 +11
	-4	1.040 +15	1.395 +6	1.081 +15	2.757 +11	9.812 +5	1.053 +11	5.042 +12
	-3	1.061 +16	2.539 +6	1.081 +16	2.673 +13	1.011 +6	3.415 +11	1.586 +14
	-2	1.054 +17	4.670 +6	1.074 +17	2.294 +15	1.163 +6	1.154 +12	4.630 +15
	-1	1.029 +18	9.684 +6	1.029 +18	1.153 +17	2.126 +6	4.875 +12	1.025 +17
	0	1.011 +19	2.571 +7	8.840 +18	2.199 +18	8.228 +6	3.006 +13	1.404 +18
5,000	-5	1.930 +13	3.172 +7	5.449 +13	3.443 +8	1.263 +9	4.532 +11	4.124 +10
	-4	5.884 +14	5.325 +8	9.518 +14	1.924 +10	6.894 +9	5.846 +12	1.702 +12
	-3	8.870 +15	2.402 +9	1.063 +16	1.572 +12	1.053 +10	2.805 +13	5.974 +13
	-2	1.007 +17	4.993 +9	1.078 +17	1.481 +14	1.149 +10	9.876 +13	1.954 +15
	-1	1.031 +18	9.375 +9	1.077 +18	1.298 +16	1.307 +10	3.371 +14	5.854 +16
	0	1.005 +19	1.871 +10	1.050 +19	7.584 +17	2.129 +10	1.343 +15	1.397 +18
6,000	-5 -3 -2 -1 0	6.547 +11 5.903 +13 3.207 +15 7.142 +16 9.336 +17 9.911 +18	4.582 +7 1.369 +9 3.179 +10 3.194 +11 9.465 +11 1.898 +12	1.877 +12 1.586 +14 6.128 +15 9.729 +16 1.063 +18 1.072 +19	8.959 +7 7.829 +9 4.667 +11 2.710 +13 2.197 +15 1.758 +17	4.374 +8 3.574 +10 8.951 +11 3.886 +12 5.724 +12 7.273 +12	4.592 +10 3.942 +12 1.454 +14 1.430 +15 6.274 +15 2.304 +16	5.481 +9 4.866 +11 2.769 +13 9.958 +14 3.242 +16 9.448 +17
7,000	-5	4.367 +10	6.421 +7	6.848 +10	2.336 +7	5.041 +7	3.884 +9	9.217 +8
	-4	4.371 +12	1.833 +9	8.553 +12	2.338 +9	7.855 +9	4.851 +11	9.226 +10
	-3	4.071 +14	5.392 +10	8.242 +14	2.184 +11	7.812 +11	4.668 +13	8.603 +12
	-2	2.513 +16	1.266 +12	4.359 +16	1.496 +13	3.189 +13	2.344 +15	5.595 +14
	-1	6.422 +17	1.399 +13	8.786 +17	8.033 +14	2.413 +14	3.259 +16	2.073 +16
	0	8.873 +18	4.877 +13	1.038 +19	5.526 +16	4.900 +14	1.726 +17	6.390 +17
8,000	-5	5.107 +9	9.149 +7	3.281 +9	7.938 +6	3.586 +6	3.475 +8	2.196 +8
	-4	5.539 +11	2.365 +9	6.693 +11	8.476 +8	1.397 +9	7.143 +10	2.363 +10
	-3	5.586 +13	6.786 +10	8.525 +13	8.540 +10	2.250 +11	9.103 +12	2.382 +12
	-2	5.100 +15	1.953 +12	8.236 +15	7.978 +12	2.248 +13	8.694 +14	2.200 +14
	-1	2.863 +17	4.093 +13	4.294 +17	5.458 +14	8.930 +14	4.106 +16	1.364 +16
	0	6.611 +18	3.675 +14	8.590 +18	2.882 +16	6.768 +15	5.431 +17	4.761 +17
9,000	-5	6.430 +8	8.693 +7	1.790 +8	2.628 +6	2.033 +5	2.906 +7	5.136 +7
	-4	9.884 +10	2.875 +9	6.543 +10	3.618 +8	1.974 +8	1.123 +10	7.472 +9
	-3	1.091 +13	8.030 +10	1.195 +13	3.885 +10	6.129 +10	2.078 +12	8.133 +11
	-2	1.095 +15	2.354 +12	1.445 +15	3.902 +12	8.923 +12	2.512 +14	8.166 +13
	-1	9.174 +16	6.369 +13	1.276 +17	3.493 +14	7.770 +14	2.146 +16	7.073 +15
	0	3.903 +18	1.026 +15	5.258 +18	2.164 +16	2.131 +16	7.331 +17	3.631 +17
10,000	-5 -4 -3 -2 -1	5.401 +7 1.876 +10 2.698 +12 2.934 +14 2.834 +16 1.888 +18	3.820 +7 2.662 +9 8.883 +10 2.626 +12 7.687 +13 1.735 +15	1.092 +7 7.234 +9 2.054 +12 3.148 +14 3.450 +16 2.414 +18	5.973 +5 1.546 +8 1.983 +10 2.098 +12 2.062 +14 1.643 +16	1.463 +4 2.481 +7 1.558 +10 3.462 +12 4.230 +14 2.600 +16	2.248 +6 1.725 +9 5.186 +11 8.060 +13 8.755 +15 5.603 +17	7.890 +6 2.365 +9 3.214 +11 3.446 +13 3.358 +15 2.446 +17
11,000	-5	2.669 +6	8.618 +6	5.839 +5	7·3 ⁴ 5 + ⁴	1.144 +3	1.394 +5	6.692 +5
	-4	2.959 +9	1.588 +9	8.762 +8	5·5 ⁴ 0 +7	3.415 +6	2.535 +8	6.119 +8
	-3	7.312 +11	8.503 +10	3.982 +11	1·0 ⁴ 8 +10	3.730 +9	1.317 +11	1.323 +11
	-2	9.379 +13	2.772 +12	8.216 +13	1·2 ₃ 0 +12	1.353 +12	2.841 +13	1.623 +13
	-1	9.803 +15	8.397 +13	1.055 +16	1·2 ₆ 7 +1 ⁴	2.165 +14	3.674 +15	1.684 +15
	0	8.292 +17	2.253 +15	9.733 +17	1·1 ₆ 1 +1 ₆	2.010 +16	3.256 +17	1.483 +17
12,000	-5	1.107 +5	1.478 +6	2.974 +4	6.094 +3	9.805 +1	8.293 +3	4.201 +4
	-4	3.495 +8	6.210 +8	1.034 +8	1.436 +7	5.028 +5	3.337 +7	1.146 +8
	-3	1.914 +11	6.540 +10	8.383 +10	5.268 +9	9.013 +8	3.306 +10	5.136 +10
	-2	3.335 +13	2.725 +12	2.426 +13	7.568 +11	5.253 +11	1.054 +13	8.126 +12
	-1	3.844 +15	8.717 +13	3.717 +15	8.263 +13	1.129 +14	1.659 +15	9.115 +14
	0	3.677 +17	2.547 +15	4.000 +17	8.111 +15	1.333 +16	1.762 +17	8.833 +16

Note: A group of digits followed by +n indicates that the decimal point should be n places to the right of the first digit.

TABLE II.- NUMBER DENSITY, MOLECULES/CM3: 50 PERCENT CO $_{\!\!2}$ - 30 PERCENT N $_{\!\!2}$ - 20 PERCENT A

Tz, °K	log ₁₀ ρ ₂ /ρ ₀	N ₂	N ₂	co	02	C ₂	CN	NO
4,000	-5 -4 -3 -2 -1 0	5.213 +13 5.779 +14 5.937 +15 5.892 +16 5.706 +17 5.569 +18	4.738 +5 9.257 +5 1.693 +6 3.095 +6 6.318 +6 1.655 +7	1.012 +14 1.014 +15 1.013 +16 1.007 +17 9.663 +17 8.311 +18	2.457 +9 2.431 +11 2.370 +13 2.073 +15 1.085 +17 2.142 +18	9.640 +5 9.788 +5 1.003 +6 1.133 +6 1.992 +6 7.466 +6	2.337 +10 7.840 +10 2.544 +11 8.518 +11 3.514 +12 2.125 +13	1.066 +11 3.529 +12 1.117 +14 3.290 +15 7.409 +16 1.028 +18
5,000	-5 -4 -3 -2 -1	7.075 +12 2.729 +14 4.675 +15 5.538 +16 5.724 +17 5.532 +18	1.190 +7 2.624 +8 1.502 +9 3.280 +9 6.175 +9 1.211 +10	4.978 +13 8.878 +14 9.970 +15 1.012 +17 1.010 +18 9.857 +18	3.082 +8 1.708 +10 1.388 +12 1.315 +14 1.177 +16 7.216 +17	1.177 +9 6.752 +9 1.049 +10 1.139 +10 1.269 +10 1.971 +10	2.649 +11 3.940 +12 2.032 +13 7.290 +13 2.474 +14 9.585 +14	2.362 +10 1.092 +12 4.075 +13 1.366 +15 4.153 +16 1.011 +18
6,000	-5 -4 -3 -2 -1	2.084 +11 1.959 +13 1.280 +15 3.512 +16 5.009 +17 5.431 +18	1.511 +7 4.687 +8 1.311 +10 1.759 +11 6.051 +11 1.231 +12	1.650 +12 1.414 +14 5.636 +15 9.106 +16 9.978 +17 1.006 +19	7.889 +7 6.942 +9 4.175 +11 2.405 +13 1.962 +15 1.623 +17	3.839 +8 3.204 +10 8.465 +11 3.837 +12 5.646 +12 6.940 +12	2.428 +10 2.150 +12 8.935 +13 9.963 +14 4.564 +15 1.666 +16	2.902 +9 2.640 +11 1.655 +13 6.578 +14 2.244 +16 6.719 +17
7,000	-5 -4 -3 -2 -1	1.382 +10 1.389 +12 1.332 +14 9.597 +15 3.059 +17 4.686 +18	2.126 +7 6.056 +8 1.829 +10 5.010 +11 7.347 +12 3.051 +13	5.945 +10 7.499 +12 7.305 +14 3.984 +16 8.229 +17 9.765 +18	2.054 +7 2.058 +9 1.930 +11 1.336 +13 7.154 +14 4.998 +16	4.320 +7 6.862 +9 6.944 +11 2.982 +13 2.377 +14 4.791 +14	2.023 +9 2.556 +11 2.518 +13 1.400 +15 2.232 +16 1.240 +17	4.862 +8 4.878 +10 4.626 +12 3.268 +14 1.350 +16 4.416 +17
8,000	-5 -4 -3 -2 -1 0	1.605 +9 1.752 +11 1.776 +13 1.683 +15 1.119 +17 3.179 +18	3.086 +7 7.870 +8 2.254 +10 6.708 +11 1.673 +13 1.985 +14	2.747 +9 5.793 +11 7.470 +13 7.311 +15 3.948 +17 8.092 +18	6.938 +6 7.447 +8 7.514 +10 7.055 +12 4.879 +14 2.580 +16	2.874 +6 1.191 +9 1.963 +11 2.003 +13 8.444 +14 6.710 +15	1.744 +8 3.710 +10 4.795 +12 4.714 +14 2.496 +16 3.751 +17	1.151 +8 1.246 +10 1.260 +12 1.188 +14 8.061 +15 3.124 +17
9,000	-5 -4 -3 -2 -1 0	1.933 +8 3.100 +10 3.451 +12 3.496 +14 3.126 +16 1.629 +18	2.892 +7 9.691 +8 2.681 +10 7.884 +11 2.268 +13 4.562 +14	1.413 +8 5.496 +10 1.035 +13 1.268 +15 1.143 +17 4.913 +18	2.222 +6 3.160 +8 3.413 +10 3.435 +12 3.100 +14 1.940 +16	1.499 +5 1.595 +8 5.240 +10 7.808 +12 7.029 +14 2.075 +16	1.368 +7 5.651 +9 1.081 +12 1.328 +14 1.191 +16 4.674 +17	2.589 +7 3.910 +9 4.288 +11 4.330 +13 3.889 +15 2.222 +17
10,000	-5 -4 -3 -2 -1 0	1.487 +7 5.694 +9 8.473 +11 9.295 +13 9.181 +15 6.915 +17	1.183 +7 8.877 +8 2.988 +10 8.793 +11 2.619 +13 6.686 +14	8.107 +6 5.820 +9 1.745 +12 2.740 +14 3.046 +16 2.212 +18	4.683 +5 1.319 +8 1.735 +10 1.844 +12 1.819 +14 1.469 +16	1.029 +4 1.881 +7 1.286 +10 2.985 +12 3.737 +14 2.440 +16	9.890 +5 8.277 +8 2.640 +11 4.213 +13 4.685 +15 3.285 +17	3.665 +6 1.204 +9 1.684 +11 1.818 +13 1.795 +15 1.400 +17
11,000	-5 -4 -3 -2 -1 0	6.765 +5 8.458 +8 2.253 +11 2.955 +13 3.125 +15 2.808 +17	2.491 +6 5.054 +8 2.847 +10 9.309 +11 2.829 +13 8.036 +14	4.078 +5 6.737 +8 3.290 +11 7.071 +13 9.242 +15 8.747 +17	5.271 +4 4.511 +7 9.052 +9 1.078 +12 1.115 +14 1.032 +16	7.776 +2 2.480 +6 2.947 +9 1.143 +12 1.888 +14 1.826 +16	1.155 +8 6.499 +10 1.466 +13 1.937 +15	2.854 +5 2.952 +8 6.826 +10 8.528 +12 8.922 +14 8.137 +16
12,000	-5 -4 -3 -2 -1 0	2.681 +4 9.323 +7 5.699 +10 1.041 +13 1.217 +15 1.200 +17	4.121 +5 1.866 +8 2.138 +10 9.138 +11 2.930 +13 8.780 +14	1.997 +4 7.558 +7 6.715 +10 2.056 +13 3.234 +15 3.550 +17	7.258 +13	6.519 +1 3.530 +5 6.857 +8 4.330 +11 9.734 +13 1.187 +16	1.444 +7 1.574 +10 5.343 +12 8.663 +14	1.703 +4 5.165 +7 2.574 +10 4.238 +12 4.806 +14 4.745 +16

TABLE III.- NUMBER DENSITY, MOLECULES/CM3: 50 PERCENT CO2 - 50 PERCENT A

Tz, oK	log ₁₀ ρ ₂ /ρ ₀	со	02	C ₂	T2, ok	$\log_{10} \rho_2/\rho_0$	CO	02	C2
4,000	-5 -4 -3 -2 -1 0	9.253 +13 9.275 +14 9.271 +15 9.218 +16 8.842 +17 7.569 +18	2.061 +9 2.049 +11 2.029 +13 1.863 +15 1.070 +17 2.248 +18	9.619 +5 9.721 +5 9.807 +5 1.056 +6 1.692 +6 5.900 +6	9,000	-5 -4 -3 -2 -1 0	9.864 +7 4.271 +10 8.468 +12 1.057 +15 9.805 +16 4.531 +18	1.730 +6 2.613 +8 2.850 +10 2.878 +12 2.625 +14 1.666 +16	9.378 +4 1.164 +8 4.197 +10 6.476 +12 6.109 +14 2.055 +16
5,000	-5 -4 -3 -2 -1	4.387 +13 8.067 +14 9.125 +15 9.259 +16 9.244 +17 9.013 +18	2.642 +8 1.448 +10 1.170 +12 1.130 +14 1.074 +16 7.449 +17	1.066 +9 6.581 +9 1.042 +10 1.110 +10 1.165 +10 1.596 +10	10,000	-5 -4 -3 -2 -1 0	5.130 +6 4.198 +9 1.381 +12 2.256 +14 2.560 +16 1.966 +18	3.213 +5 1.047 +8 1.438 +10 1.540 +12 1.529 +14 1.259 +16	6.002 +3 1.234 +7 9.718 +9 2.421 +12 3.141 +14 2.249 +16
6,000	-5 -4 -3 -2 -1 0	1.379 +12 1.204 +14 5.021 +15 8.343 +16 9.161 +17 9.219 +18	6.610 +7 5.871 +9 3.573 +11 2.033 +13 1.706 +15 1.556 +17	3.202 +8 2.749 +10 7.851 +11 3.810 +12 5.475 +12 6.077 +12	11,000	-5 -4 -3 -2 -1 0	2.358 +5 4.513 +8 2.483 +11 5.714 +13 7.678 +15 7.537 +17	3.164 +4 3.300 +7 7.344 +9 8.965 +11 9.336 +13 8.765 +15	4.330 +2 1.521 +6 2.069 +9 8.975 +11 1.556 +14 1.597 +16
7,000	-5 -4 -3 -2 -1 0	4.877 +10 6.244 +12 6.173 +14 3.520 +16 7.583 +17 9.030 +18	1.717 +7 1.723 +9 1.625 +11 1.142 +13 6.069 +14 4.476 +16	3.478 +7 5.683 +9 5.889 +11 2.725 +13 2.379 +14 4.575 +14	12,000	-5 -4 -3 -2 -1 0	1.093 +4 4.680 +7 4.814 +10 1.620 +13 2.658 +15 3.002 +17	2.294 +3 7.184 +6 3.455 +9 5.435 +11 6.059 +13 6.050 +15	3.521 +1 2.060 +5 4.532 +8 3.261 +11 7.879 +13 1.007 +16
8,000	-5 -4 -3 -2 -1 0	2.125 +9 4.729 +11 6.213 +13 6.191 +15 3.528 +17 7.579 +18	5.746 +6 6.222 +8 6.291 +10 5.944 +12 4.174 +14 2.209 +16	2.078 +6 9.502 +8 1.622 +11 1.705 +13 7.883 +14 6.875 +15					

TABLE IV.- NUMBER DENSITY, MOLECULES/CM3: 100 PERCENT CO2

T2, oK	log 10 ρ ₂ /ρ ₀	со	02	Ca	T2, °K	log ₁₀ ρ ₂ /ρ ₀	CO	02	C2
4,000	-5 -4 -3 -2 -1	1.767 +14 1.769 +15 1.768 +16 1.749 +17 1.639 +18 1.340 +19	7.479 +9 7.446 +11 7.317 +13 6.276 +15 2.788 +17 4.523 +18	9.669 +5 9.733 +5 9.885 +5 1.128 +6 2.232 +6 9.197 +6	9,000	-5 -4 -3 -2 -1 0	5.417 +8 1.984 +11 3.370 +13 3.897 +15 3.171 +17 1.102 +19	7.343 +6 9.865 +8 1.045 +11 1.038 +13 8.826 +14 5.012 +6	6.666 +5 6.655 +8 1.813 +11 2.440 +13 1.900 +15 4.045 +16
5,000	-5 -4 -3 -2 -1 0	1.079 +14 1.635 +15 1.754 +16 1.767 +17 1.758 +18 1.687 +19	7.970 +8 4.774 +10 4.190 +12 4.086 +14 3.731 +16 2.107 +18	2.136 +9 8.194 +9 1.075 +10 1.119 +10 1.213 +10 1.977 +10	10,000	-5 -4 -3 -2 -1	2.973 +7 2.148 +10 5.979 +12 8.698 +14 9.144 +16 5.745 +18	1.617 +6 4.277 +8 5.381 +10 5.631 +12 5.437 +14 4.015 +16	4.006 +4 7.906 +7 4.869 +10 9.846 +12 1.127 +15 6.024 +16
6,000	-5 -4 -3 -2 -1	5.014 +12 3.798 +14 1.190 +16 1.668 +17 1.757 +18 1.752 +19	2.374 +8 1.947 +10 1.077 +12 6.823 +13 6.092 +15 5.301 +17	1.179 +9 8.243 +10 1.462 +12 4.535 +12 5.636 +12 6.443 +12	11,000	-5 -4 -3 -2 -1 0	1.517 +6 2.416 +9 1.160 +12 2.310 +14 2.860 +16 2.500 +18	1.915 +5 1.508 +8 2.871 +10 3.319 +12 3.386 +14 2.992 +16	2.960 +3 9.537 +6 1.155 +10 3.963 +12 5.954 +14 5.148 +16
7,000	-5 -4 -3 -2 -1 0	1.964 +11 2.325 +13 2.087 +15 9.147 +16 1.573 +18 1.741 +19	6.270 +7 6.235 +9 5.605 +11 3.480 +13 1.945 +15 1.562 +17	1.544 +8 2.177 +10 1.951 +12 6.037 +13 3.195 +14 4.871 +14	12,000	-5 -4 -3 -2 -1 0	7.666 +4 2.708 +8 2.352 +11 6.872 +13 1.019 +16 1.063 +18	1.573 +4 3.781 +7 1.440 +10 2.055 +12 2.221 +14 2.144 +16	2.524 +2 1.311 +6 2.595 +9 1.553 +12 3.160 +14 3.559 +16
8,000	-5 -4 -3 -2 -1 0	1.034 +10 1.920 +12 2.320 +14 2.094 +16 9.158 +17 1.571 +19	2.166 +7 2.279 +9 2.279 +11 2.050 +13 1.271 +15 7.045 +16	1.305 +7 4.275 +9 6.246 +11 5.652 +13 1.744 +15 9.264 +15					

TABLE V.- NUMBER DENSITY, MOLECULES/CM3: 100 PERCENT N2

			+	- O			+
T ₂ , ^O K	$\log_{10} \rho_2/\rho_0$	N ₂	N_2^+	T ₂ , ^O K	$\log_{10} \rho_2/\rho_0$	N ₂	N ₂
4,000	-5 -4 -3 -2 -1 0	2.588 +14 2.718 +15 2.761 +16 2.774 +17 2.778 +18 2.780 +19	6.689 +7 3.105 +8 1.202 +9 4.129 +9 1.344 +10 4.292 +10	9,000	-5 -4 -3 -2 -1 0	3.864 +9 6.066 +11 6.971 +13 6.967 +15 4.999 +17 1.524 +19	6.258 +8 2.776 +10 9.739 +11 3.071 +13 7.424 +14 8.804 +15
5,000	-5 -4 -3 -2 -1 0	8.842 +13 1.901 +15 2.464 +16 2.676 +17 2.747 +18 2.770 +19	1.314 +9 1.260 +10 7.677 +10 3.574 +11 1.367 +12 4.661 +12	10,000	-5 -4 -3 -2 -1 0	3.501 +8 1.142 +11 1.685 +13 1.883 +15 1.742 +17 9.086 +18	2.518 +8 1.934 +10 8.182 +11 2.810 +13 8.320 +14 1.535 +16
6,000	-5 -4 -3 -2 -1 0	4.234 +12 3.380 +14 1.279 +16 2.163 +17 2.568 +18 2.711 +19	1.630 +9 4.331 +10 6.424 +11 4.884 +12 2.512 +13 1.011 +14	11,000	-5 -4 -3 -2 -1 0	1.845 +7 1.895 +10 4.520 +12 5.962 +14 6.251 +16 4.656 +18	5.800 +7 1.052 +10 6.387 +11 2.485 +13 8.115 +14 2.003 +16
7,000	-5 -4 -3 -2 -1 0		1.304 +9 4.145 +10 1.162 +12 1.948 +13 1.584 +14 8.182 +14	12,000	-5 -4 -3 -2 -1 0	7.756 +5 2.381 +9 1.209 +12 2.102 +14 2.468 +16 2.242 +18	1.004 +7 4.141 +9 4.429 +11 2.121 +13 7.552 +14 2.191 +16
8,000	-5 -4 -3 -2 -1	3.109 +10 3.534 +12 3.597 +14 2.981 +16 1.205 +18 2.120 +19	9.992 +8 3.478 +10 1.113 +12 3.032 +13 4.631 +14 3.425 +15	1	;		I

TABLE VI.- NUMBER DENSITY, MOLECULES/CM 3 : 25 PERCENT CO $_2$ - 75 PERCENT N $_2$

T2, °K	$\log_{10} \rho_2/\rho_0$	N ₂	N ₂	со	02	C2	CN	NO
4,000	-5	1.669 +14	1.467 +6	6.054 +13	8.860 +8	9.576 +5	4.168 +10	1.145 +11
	-4	1.772 +15	2.775 +6	6.079 +14	8.708 +10	9.824 +5	1.375 +11	3.699 +12
	-3	1.803 +16	5.043 +6	6.079 +15	8.424 +12	1.016 +6	4.461 +11	1.160 +14
	-2	1.803 +17	9.270 +6	6.058 +16	7.380 +14	1.151 +6	1.502 +12	3.434 +15
	-1	1.782 +18	1.876 +7	5.899 +17	4.257 +16	1.893 +6	6.054 +12	8.200 +16
	0	1.762 +19	4.754 +7	5.288 +18	9.969 +17	6.493 +6	3.526 +13	1.248 +18
5,000	-5	4.578 +13	8.944 +7	2.315 +13	1.276 +8	6.150 +8	4.871 +11	3.866 +10
	-4	1.140 +15	1.114 +9	4.936 +14	6.847 +9	5.208 +9	7.072 +12	1.413 +12
	-3	1.568 +16	4.831 +9	5.898 +15	5.090 +11	1.000 +10	3.636 +13	4.520 +13
	-2	1.733 +17	1.001 +10	6.053 +16	4.668 +13	1.149 +10	1.295 +14	1.439 +15
	-1	1.776 +18	1.883 +10	6.063 +17	4.073 +15	1.321 +10	4.447 +14	4.303 +16
	0	1.763 +19	3.746 +10	5.978 +18	2.548 +17	2.053 +10	1.746 +15	1.072 +18
6,000	-5	1.849 +12	1.713 +8	5.881 +11	2.855 +7	1.348 +8	4.284 +10	5.200 +9
	-4	1.573 +14	4.665 +9	5.465 +13	2.630 +9	1.264 +10	3.826 +12	4.603 +11
	-3	7.027 +15	8.084 +10	2.678 +15	1.745 +11	4.573 +11	1.539 +14	2.506 +13
	-2	1.328 +17	6.476 +11	5.082 +16	9.545 +12	3.010 +12	1.716 +15	8.059 +14
	-1	1.638 +18	1.910 +12	5.888 +17	7.051 +14	5.471 +12	8.126 +15	2.433 +16
	0	1.733 +19	3.861 +12	6.021 +18	5.478 +16	7.363 +12	3.066 +16	6.974 +17
7,000	-5 -4 -3 -2 -1	1.238 +11 1.237 +13 1.107 +15 5.760 +16 1.228 +18 1.584 +19	2.429 +8 6.783 +9 1.876 +11 3.449 +12 2.916 +13 9.872 +13	1.974 +10 2.634 +12 2.706 +14 1.734 +16 4.332 +17 5.631 +18	7.364 +6 7.415 +8 7.130 +10 5.437 +12 2.953 +14 1.815 +16	1.329 +7 2.350 +9 2.578 +11 1.389 +13 1.596 +14 4.386 +14	3·357 +9 4·463 +11 4·422 +13 2·341 +15 3·664 +16 2·182 +17	8.711 +8 8.739 +10 8.106 +12 5.106 +14 1.737 +16 4.894 +17
8,000	-5	1.416 +10	3.171 +8	8.840 +8	2.458 +6	8.404 +5	2.801 +8	2.035 +8
	-4	1.564 +12	8.571 +9	1.944 +11	2.666 +8	3.747 +8	6.217 +10	2.228 +10
	-3	1.577 +14	2.438 +11	2.628 +13	2.706 +10	6.747 +10	8.375 +12	2.253 +12
	-2	1.373 +16	6.572 +12	2.697 +15	2.602 +12	7.389 +12	8.179 +14	2.062 +14
	-1	6.456 +17	1.078 +14	1.687 +17	1.978 +14	3.804 +14	4.024 +16	1.233 +16
	0	1.264 +19	7.629 +14	4.151 +18	1.062 +16	4.288 +15	5.979 +17	3.998 +17
9,000	-5	1.758 +9	2.575 +8	5.199 +7	8.059 +5	5.595 +4	2.521 +7	4.702 +7
	-4	2.743 +11	9.530 +9	1.843 +10	1.124 +8	5.044 +7	9.456 +9	6.937 +9
	-3	3.077 +13	2.789 +11	3.558 +12	1.222 +10	1.727 +10	1.853 +12	7.663 +11
	-2	3.072 +15	8.125 +12	4.504 +14	1.239 +12	2.731 +12	2.328 +14	7.707 +13
	-1	2.385 +17	1.997 +14	4.267 +16	1.156 +14	2.628 +14	2.012 +16	6.559 +15
	0	8.396 +18	2.474 +15	2.137 +18	7.960 +15	9.565 +15	7.204 +17	3.230 +17
10,000	-5	1.524 +8	1.086 +8	3.418 +6	1.876 +5	4.563 +3	2.109 +6	7.429 +6
	-4	5.158 +10	7.912 +9	2.126 +9	4.771 +7	6.944 +6	1.514 +9	2.179 +9
	-3	7.532 +12	2.885 +11	6.008 +11	6.192 +9	4.272 +9	4.537 +11	3.000 +11
	-2	8.274 +14	8.806 +12	9.614 +13	6.613 +11	1.024 +12	7.362 +13	3.250 +13
	-1	7.820 +16	2.521 +14	1.094 +16	6.588 +13	1.331 +14	8.158 +15	3.153 +15
	0	4.586 +18	4.854 +15	8.475 +17	5.615 +15	9.374 +15	5.244 +17	2.229 +17
11,000	-5	7.752 +6	2.473 +7	1.886 +5	2.366 +4	3.704 +2	1.351 +5	6.473 +5
	-4	8.306 +9	4.527 +9	2.720 +8	1.734 +7	1.052 +6	2.357 +8	5.736 +8
	-3	2.025 +12	2.562 +11	1.182 +11	3.255 +9	1.059 +9	1.168 +11	1.227 +11
	-2	2.634 +14	8.880 +12	2.482 +13	3.859 +11	3.933 +11	2.567 +13	1.524 +13
	-1	2.752 +16	2.723 +14	3.287 +15	4.008 +13	6.643 +13	3.410 +15	1.587 +15
	0	2.187 +18	6.812 +15	3.176 +17	3.781 +15	6.574 +15	3.024 +17	1.374 +17
12,000	-5	3.23 ¹ / ₄ +5	4.259 +6	9.654 +3	1.976 +3	3.186 +1	8.081 +3	4.089 +4
	-4	1.009 +9	1.775 +9	3.318 +7	4.594 +6	1.619 +5	3.217 +7	1.101 +8
	-3	5.3 ¹ / ₄ 0 +11	1.883 +11	2.571 +10	1.644 +9	2.717 +8	3.032 +10	4.792 +10
	-2	9.320 +13	8.313 +12	7.332 +12	2.367 +11	1.535 +11	9.520 +12	7.597 +12
	-1	1.083 +16	2.750 +14	1.149 +15	2.604 +13	3.427 +13	1.533 +15	8.588 +14
	0	1.010 +18	7.867 +15	1.270 +17	2.588 +15	4.209 +15	1.641 +17	8.270 +16

TABLE VII.- NUMBER DENSITY, MOLECULES/CM3: 75 PERCENT CO2 - 25 PERCENT N2

T2, °K	log ₁₀ ρ ₂ /ρ ₀	N ₂	N ₂	co	02	C ₂	CN	NO
4,000	-5	4.092 +13	3.301 +5	1.457 +14	5.084 +9	9.671 +5	2.074 +10	1.358 +11
	-4	4.587 +14	6.488 +5	1.460 +15	5.039 +11	9.789 +5	6.985 +10	4.526 +12
	-3	4.713 +15	1.187 +6	1.458 +16	4.900 +13	1.005 +6	2.269 +11	1.431 +14
	-2	4.634 +16	2.172 +6	1.446 +17	4.159 +15	1.164 +6	7.656 +11	4.133 +15
	-1	4.425 +17	4.526 +6	1.370 +18	1.922 +17	2.260 +6	3.296 +12	8.682 +16
	0	4.303 +18	1.224 +7	1.146 +19	3.306 +18	9.199 +6	2.074 +13	1.123 +18
5,000	-5 -4 -3 -2 -1 0	4.719 +12 1.994 +14 3.618 +15 4.355 +16 4.468 +17 4.221 +18	7.186 +6 1.829 +8 1.046 +9 2.284 +9 4.289 +9 8.448 +9	8.303 +13 1.326 +15 1.443 +16 1.457 +17 1.452 +18 1.404 +19	5.745 +8 3.339 +10 2.848 +12 2.723 +14 2.406 +16 1.352 +18	1.757 +9 7.703 +9 1.070 +10 1.141 +10 1.283 +10 2.136 +10	2.643 +11 3.597 +12 1.806 +13 6.471 +13 2.198 +14 8.716 +14	2.634 +10 1.305 +12 5.136 +13 1.742 +15 5.246 +16 1.208 +18
6,000	-5	1.335 +11	8.064 +6	3.420 +12	1.623 +8	8.018 +8	2.807 +10	3.331 +9
	-4	1.267 +13	2.598 +8	2.713 +14	1.368 +10	5.988 +10	2.364 +12	2.980 +11
	-3	8.780 +14	8.228 +9	9.219 +15	7.770 +11	1.217 +12	8.871 +13	1.870 +13
	-2	2.627 +16	1.232 +11	1.352 +17	4.738 +13	4.291 +12	9.112 +14	7.986 +14
	-1	3.876 +17	4.184 +11	1.443 +18	4.031 +15	5.750 +12	4.052 +15	2.829 +16
	0	4.167 +18	8.451 +11	1.446 +19	3.305 +17	7.043 +12	1.470 +16	8.400 +17
7,000	5 1 1 1 1 1 0	8.863 +9 8.894 +11 8.576 +13 6.448 +15 2.243 +17 3.563 +18	1.114 +7 3.228 +8 9.992 +9 3.018 +11 5.063 +12 2.096 +13	1.303 +11 1.575 +13 1.456 +15 6.879 +16 1.253 +18 1.422 +19	4.264 +7 4.252 +9 3.886 +11 2.508 +13 1.371 +15 1.014 +17	9.999 +7 1.464 +10 1.370 +12 4.738 +13 2.875 +14 5.002 +14	2.464 +9 2.987 +11 2.838 +13 1.447 +15 2.102 +16 1.105 +17	5.610 +8 5.612 +10 5.268 +12 3.670 +14 1.600 +16 5.486 +17
8,000	-5 -4 -3 -2 -1 0	1.049 +9 1.126 +11 1.138 +13 1.084 +15 7.532 +16 2.317 +18	1.625 +7 4.165 +8 1.209 +10 3.685 +11 1.015 +13 1.359 +14	6.595 +9 1.273 +12 1.570 +14 1.458 +16 6.835 +17 1.238 +19	1.464 +7 1.549 +9 1.554 +11 1.421 +13 9.159 +14 4.926 +16	7.856 +6 2.767 +9 4.197 +11 3.958 +13 1.348 +15 8.230 +15	2.331 +8 4.533 +10 5.612 +12 5.319 +14 2.588 +16 3.546 +17	1.352 +8 1.441 +10 1.451 +12 1.354 +14 9.060 +15 3.685 +17
9,000	-5	1.343 +8	1.702 +7	3.491 +8	4.905 +6	4.144 +5	1.897 +7	3.207 +7
	-4	2.032 +10	5.238 +8	1.284 +11	6.666 +8	4.124 +8	7.359 +9	4.599 +9
	-3	2.221 +12	1.442 +10	2.248 +13	7.099 +10	1.188 +11	1.306 +12	4.961 +11
	-2	2.242 +14	4.276 +11	2.647 +15	7.088 +12	1.649 +13	1.546 +14	4.980 +13
	-1	2.020 +16	1.270 +13	2.229 +17	6.160 +14	1.345 +15	1.325 +16	4.407 +15
	0	1.110 +18	2.864 +14	8.255 +18	3.615 +16	3.145 +16	4.749 +17	2.502 +17
10,000	-5	1.102 +7	7.744 +6	2.008 +7	1.095 +6	2.699 +4	1.379 +6	4.826 +6
	-4	3.900 +9	5.202 +8	1.397 +10	2.870 +8	4.981 +7	1.115 +9	1.470 +9
	-3	5.531 +11	1.642 +10	3.933 +12	3.643 +10	3.112 +10	3.318 +11	1.972 +11
	-2	5.978 +13	4.803 +11	5.849 +14	3.829 +12	6.546 +12	5.003 +13	2.102 +13
	-1	5.888 +15	1.443 +13	6.256 +16	3.726 +14	7.696 +14	5.383 +15	2.058 +15
	0	4.498 +17	3.882 +14	4.104 +18	2.840 +16	4.346 +16	3.536 +17	1.570 +17
11,000	-5	5.320 +5	1.734 +6	1.047 +6	1.319 +5	2.046 +3	8.322 +4	4.004 +5
	-4	6.064 +8	3.214 +8	1.622 +9	1.019 +8	6.368 +6	1.567 +8	3.756 +8
	-3	1.511 +11	1.647 +10	7.611 +11	1.935 +10	7.378 +9	8.421 +10	8.171 +10
	-2	1.916 +13	5.179 +11	1.542 +14	2.252 +12	2.601 +12	1.780 +13	9.927 +12
	-1	2.006 +15	1.568 +13	1.938 +16	2.307 +14	4.011 +14	2.263 +15	1.028 +15
	0	1.799 +17	4.531 +14	1.733 +18	2.071 +16	3.572 +16	2.022 +17	9.225 +16
12,000	-5 -4 -3 -2 -1 0	2.196 +4 7.000 +7 3.939 +10 6.842 +12 7.842 +14 7.670 +16	2.964 +5 1.253 +8 1.312 +10 5.239 +11 1.647 +13 4.944 +14	5.308 +4 1.862 +8 1.567 +11 4.566 +13 6.870 +15 7.261 +17	1.089 +4 2.594 +7 9.710 +9 1.390 +12 1.509 +14 1.468 +16	1.749 +2 9.031 +5 1.709 +9 1.013 +12 2.113 +14 2.427 +16	2.066 +10 6.628 +12 1.025 +15	2.501 +4 6.892 +7 3.163 +10 4.989 +12 5.565 +14 5.427 +16

TABLE VIII.- VALUES AND REFERENCES FOR f NUMBERS AND FRANCK-CONDON FACTORS USED IN CALCULATIONS

Pand great on	f	number	Franck-Condon factors
Band system	Value	Reference	Reference
CN(V) CN(R) CO(4+) C ₂ (S) NO(β) NO(γ) N ₂ (1+) N ₂ (2+) N ₂ (1-) O ₂ (S-R)	0.020 ^a .007 .15 .03 ⁴ .0015 .002 ⁴ .003 ⁴ .057 .053 .16	7 21 22 24 26 26 28 30 30 31	20 20 23 25 27 27 29 29 29

aThe CN concentrations used to deduce this f value are from the same source as those given in tables I to VII.

TABLE IX.- TOTAL INTENSITY, W/PARTICLE

T2, OK Band system	4,000	5,000	6,000	7,000	8,000	9,000	10,000	11,000	12,000	Spectral range, µ
CN(V) CN(R) CO(¼+) C ₂ (S) NO(β) NO(γ) N ₂ (1+) N ₂ (2+) N ₂ (1-) O ₂ (S-R)	3.60 -16 2.27 -15 4.68 -20 2.03 -15 6.70 -20 2.01 -19 9.51 -23 1.50 -24 9.10 -16 1.71 -18	2.07 -15 4.16 -15 4.88 -18 7.68 -15 1.70 -18 4.80 -18 8.57 -21 9.30 -22 5.26 -15 5.21 -17	6.36 -15 6.03 -15 1.06 -16 1.80 -14 1.45 -17 3.96 -17 1.77 -19 6.65 -20 1.62 -14 4.81 -16	9.44 -16 3.23 -14 6.55 -17 1.78 -16 1.55 -18 1.39 -18	2.35 -14 9.08 -15 4.80 -15 4.89 -14 2.00 -16 5.48 -16 7.93 -18 1.35 -17 5.99 -14 6.91 -15	3.50 -14 1.02 -14 1.67 -14 6.63 -14 4.71 -16 1.31 -15 2.79 -17 7.76 -17 8.96 -14 1.60 -14	4.75 -14 1.10 -14 4.46 -14 8.32 -14 9.20 -16 2.61 -15 7.87 -17 3.11 -16 1.22 -13 3.06 -14	9.84 -14 9.86 -14 1.57 -15 4.57 -15 1.83 -16 9.63 -16 1.54 -13	7.23 -14 1.21 -14 1.86 -13 1.12 -13 2.42 -15 7.24 -15 3.69 -16 2.43 -15 1.86 -13 7.54 -14	0.3473 -0.4600 .4331 -1.6111 .11612913 .42586670 .15886631 .14143451 .4642 -1.2463 .25835452 .29715860 .17594668

Note: A group of digits followed by -n indicates that the decimal point should be n places to the left of the first digit.



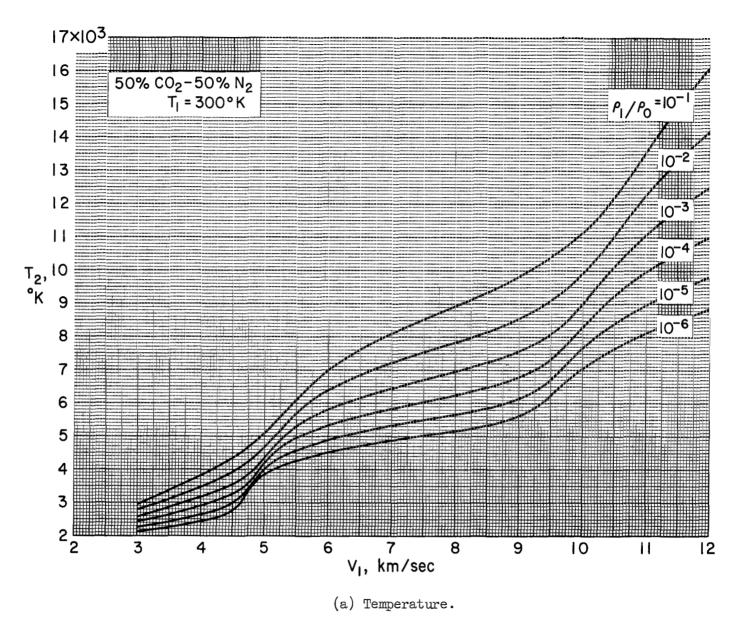
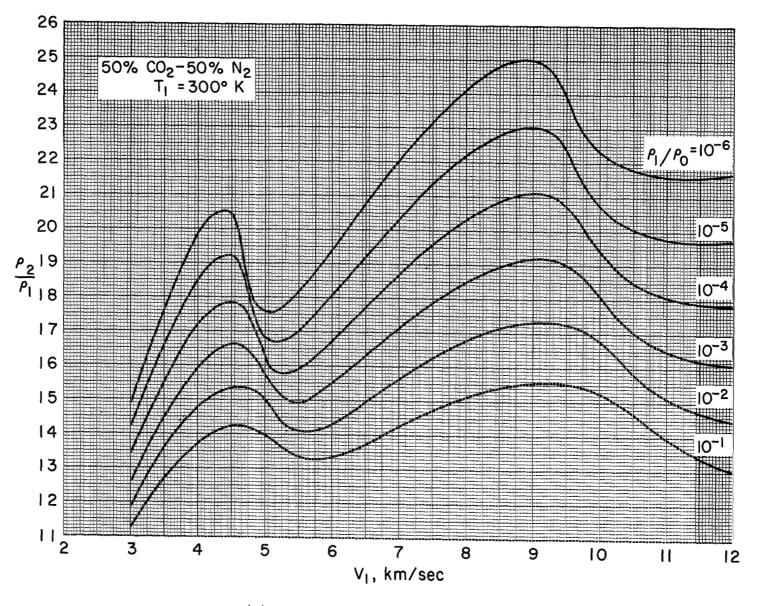


Figure 1.- Equilibrium gas properties behind normal shock waves in 0.5 $\rm CO_2$ -0.5 $\rm N_2$ mixture; $\rm T_1$ = 300° K.



(b) Density ratio across normal shock.

Figure 1.- Concluded.

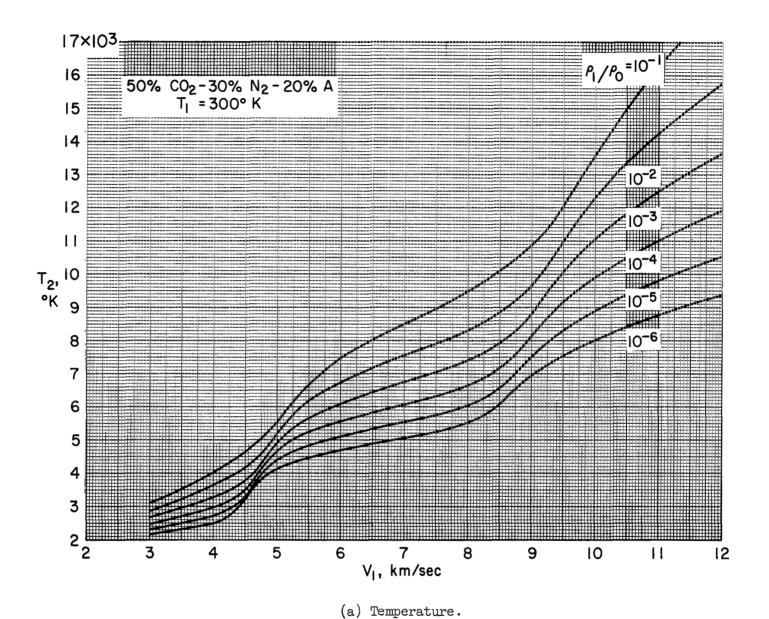


Figure 2.- Equilibrium gas properties behind normal shock waves in 0.5 CO₂-0.3 N₂-0.2 A mixture; $T_1 = 300^{\circ}$ K.

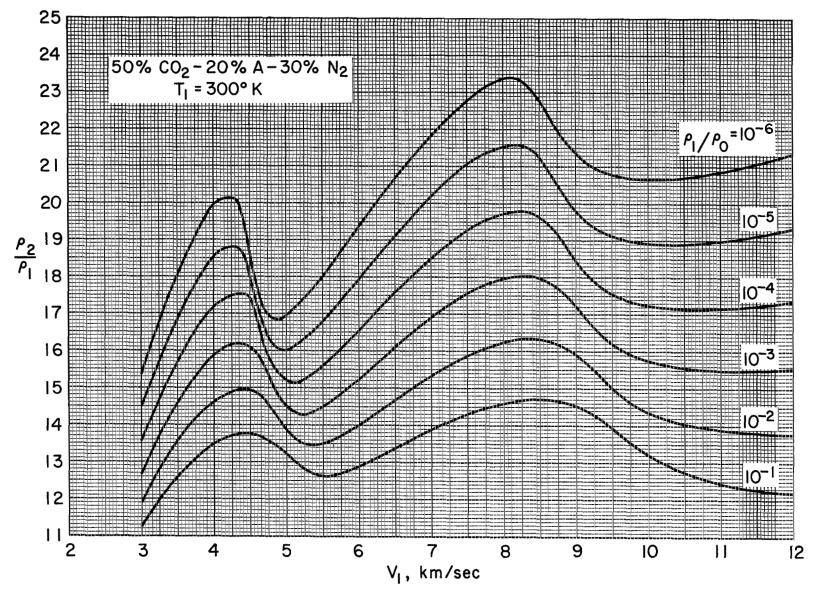


Figure 2.- Concluded.

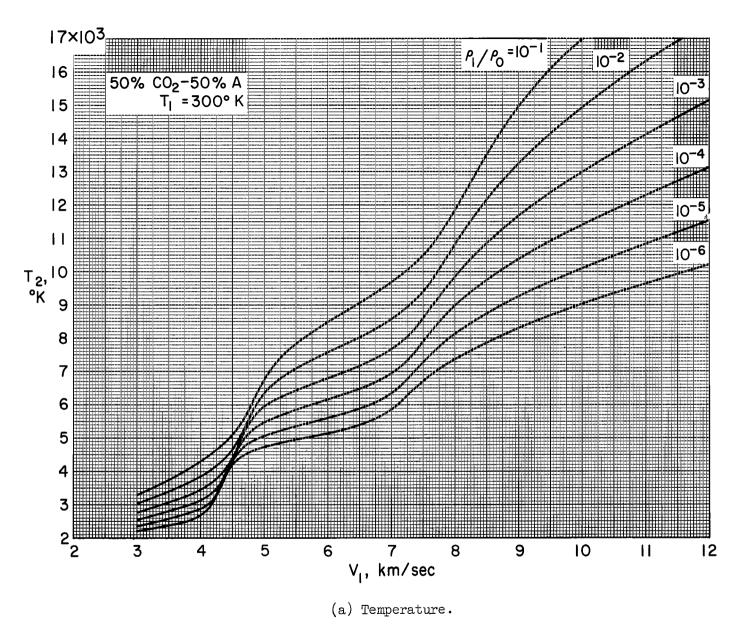
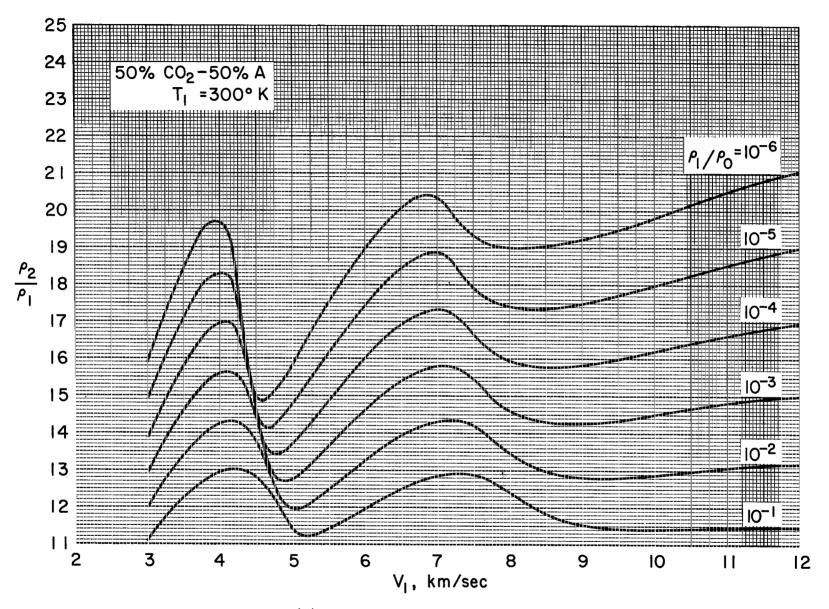


Figure 3.- Equilibrium gas properties behind normal shock waves in 0.5 $\rm CO_2$ -0.5 A mixture; $\rm T_1$ = 300° K.



(b) Density ratio across normal shock.

Figure 3.- Concluded.

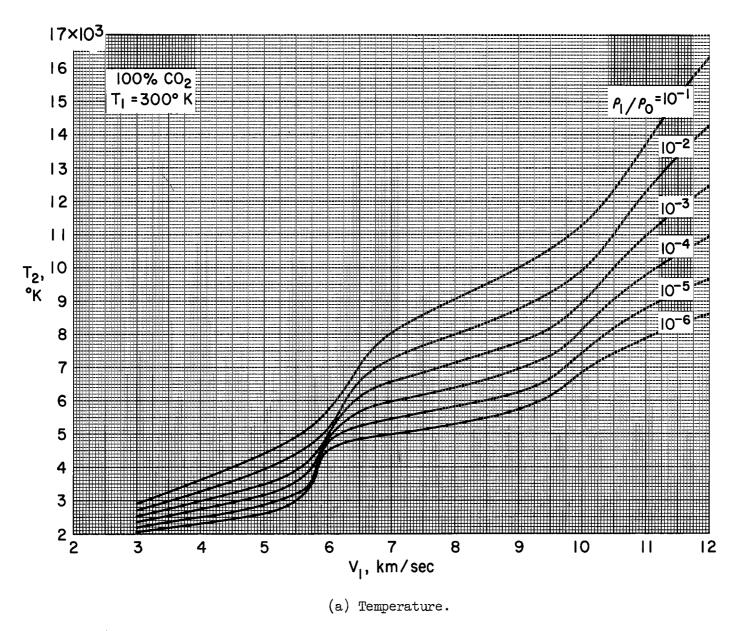


Figure 4.- Equilibrium gas properties behind normal shock waves in 1.0 $\rm CO_2$; $\rm T_1 = 300^{\circ}~K$.

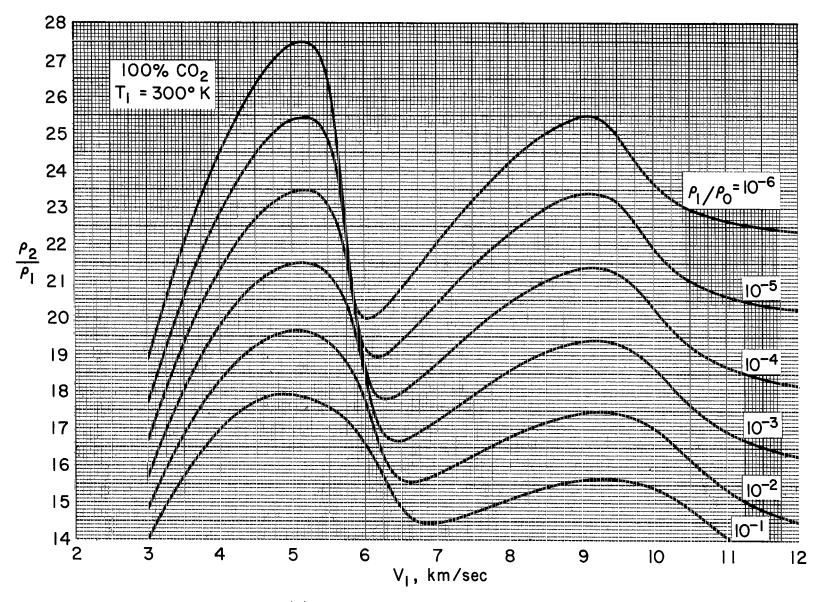


Figure 4.- Concluded.

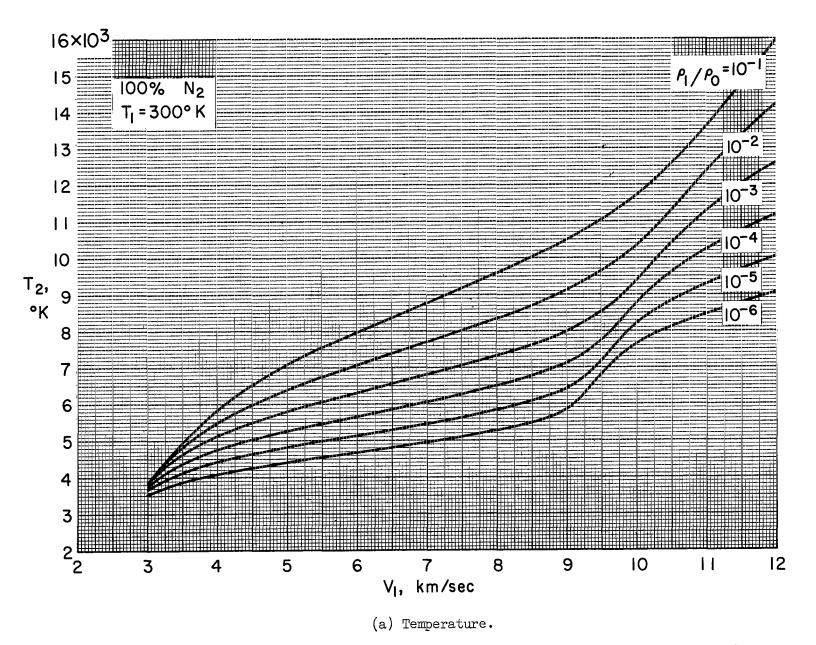


Figure 5.- Equilibrium gas properties behind normal shock waves in 1.0 N₂; $T_1 = 300^{\circ}$ K.

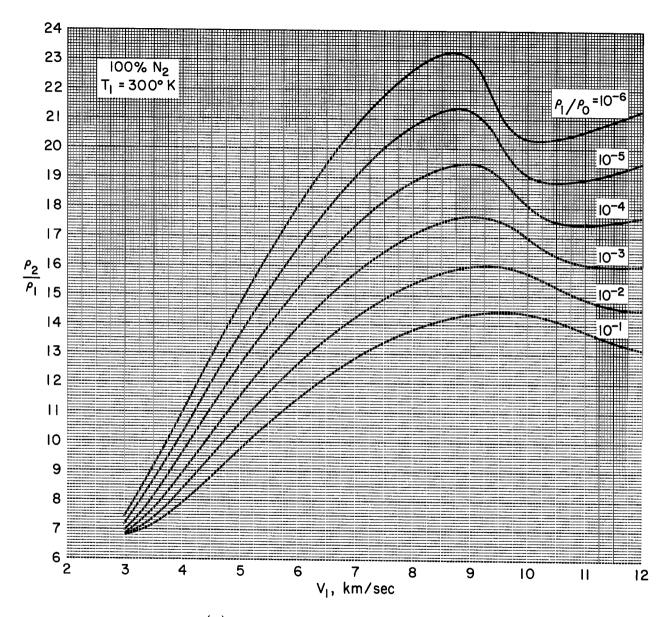
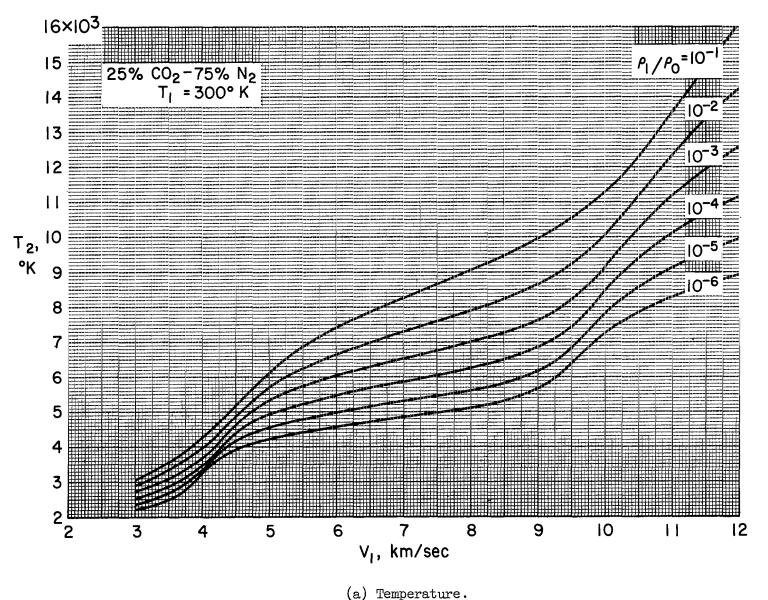
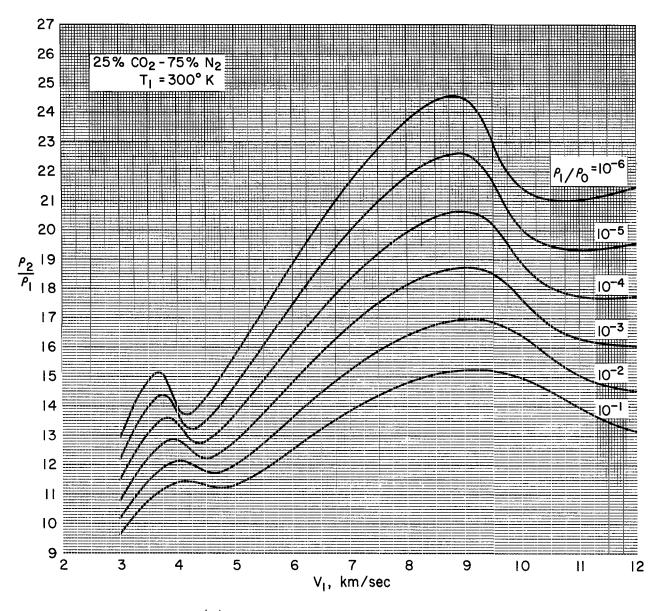


Figure 5.- Concluded.



(a) Temperature.

Figure 6.- Equilibrium gas properties behind normal shock waves in 0.25 $\rm CO_2$ -0.75 $\rm N_2$ mixture; $\rm T_1$ = 300° K.



(b) Density ratio across normal shock.

Figure 6.- Concluded.

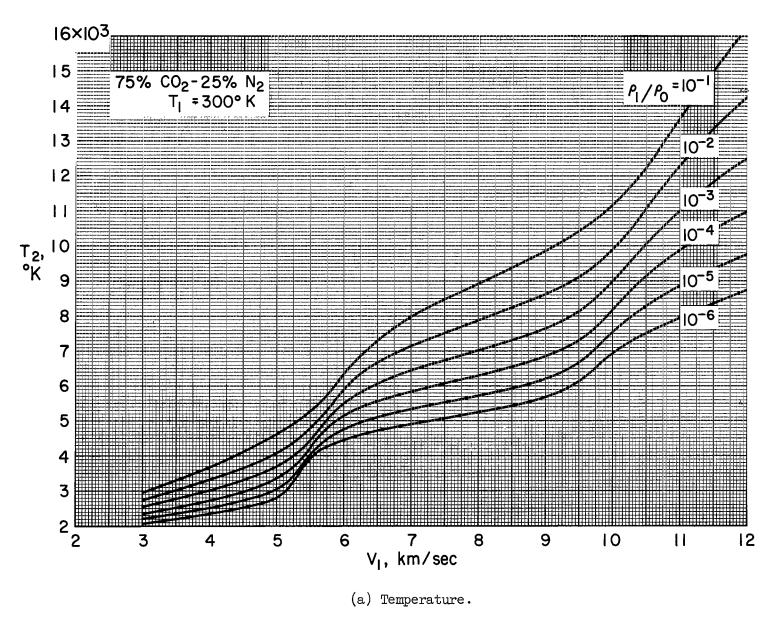


Figure 7.- Equilibrium gas properties behind normal shock waves in 0.75 CO₂-0.25 N₂ mixture; $T_1 = 300^{\circ}$ K.

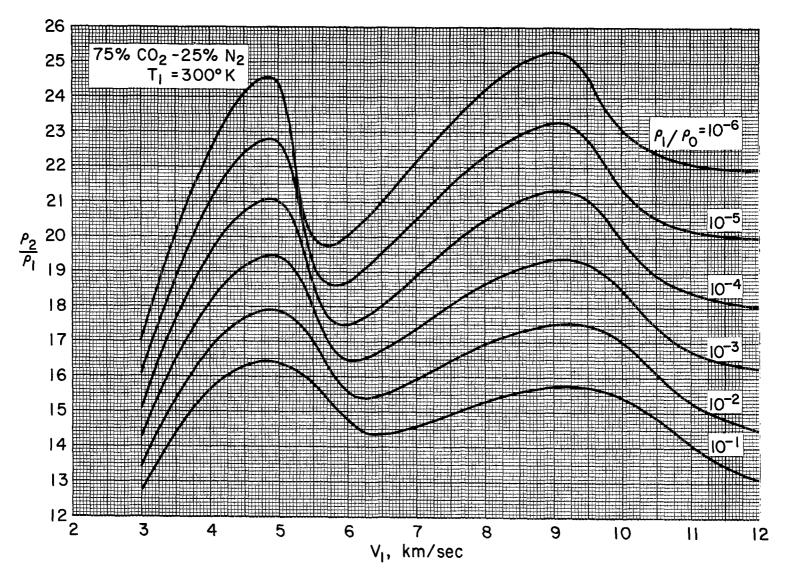


Figure 7.- Concluded.

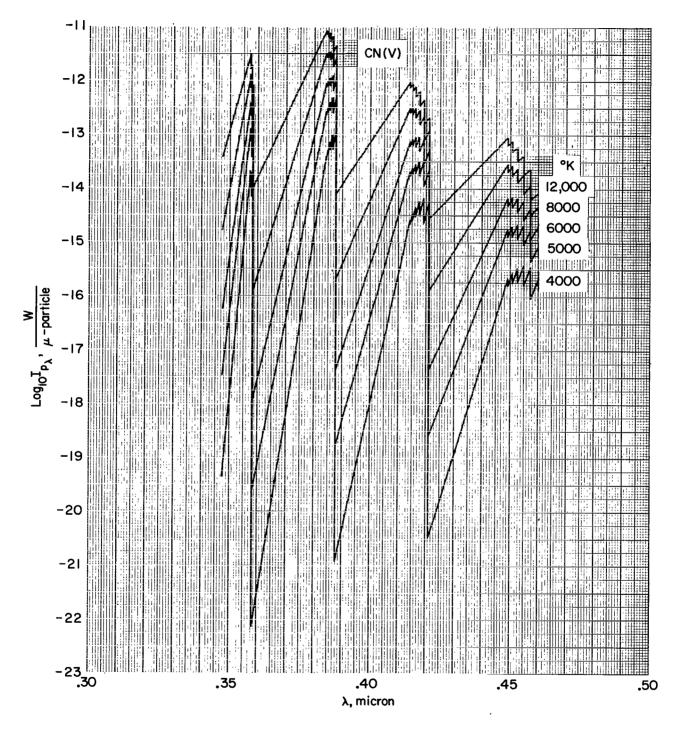


Figure 8.- Spectral intensity per particle for ${\tt CN(V)}$ band system.

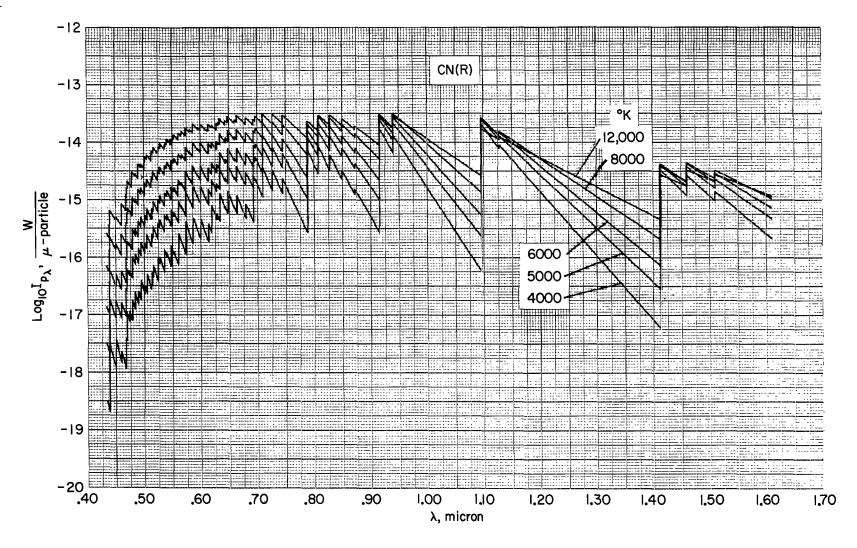


Figure 9.- Spectral intensity per particle for CN(R) band system.

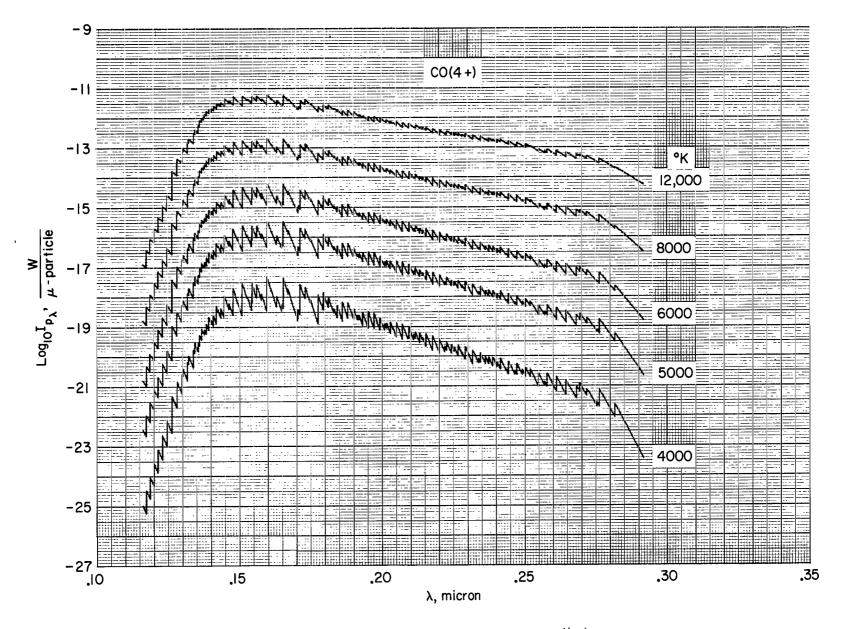


Figure 10.- Spectral intensity per particle for CO(4+) band system.

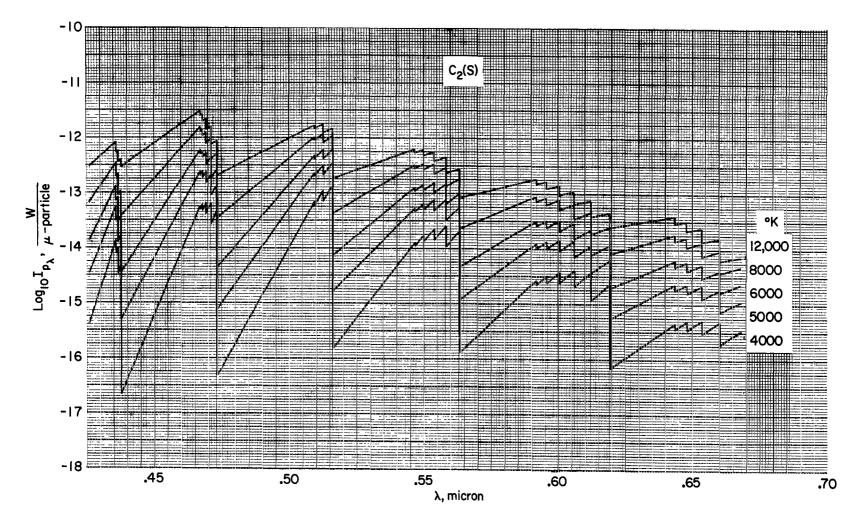


Figure 11.- Spectral intensity per particle for $C_2(S)$ band system.

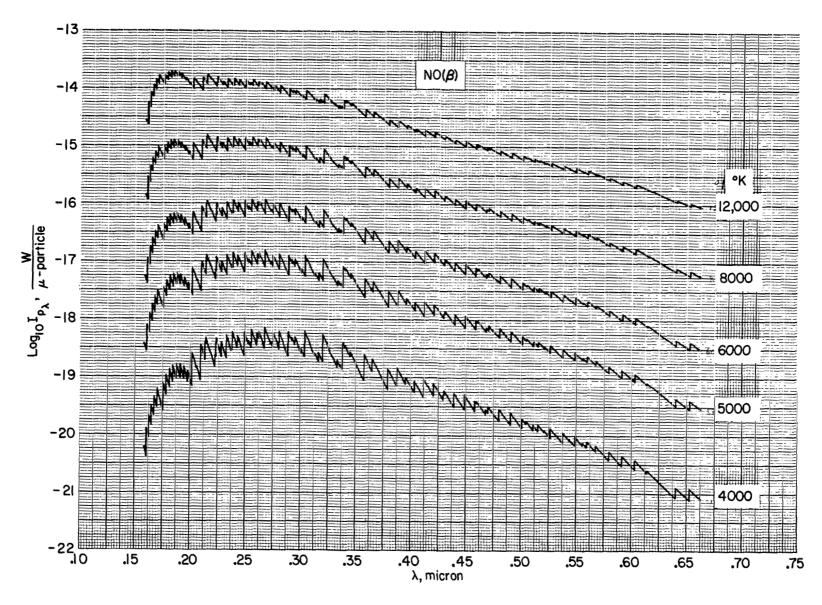


Figure 12.- Spectral intensity per particle for NO(β) band system.

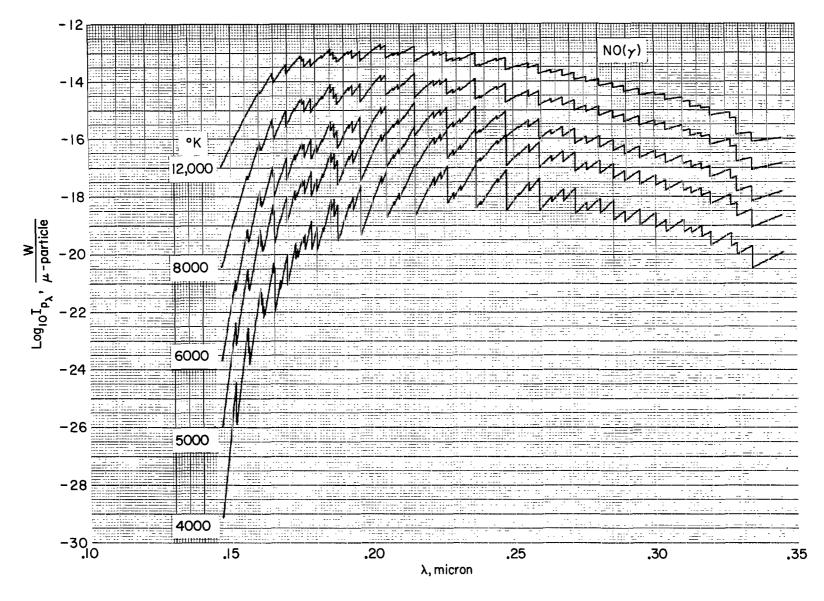


Figure 13.- Spectral intensity per particle for $NO(\gamma)$ band system.

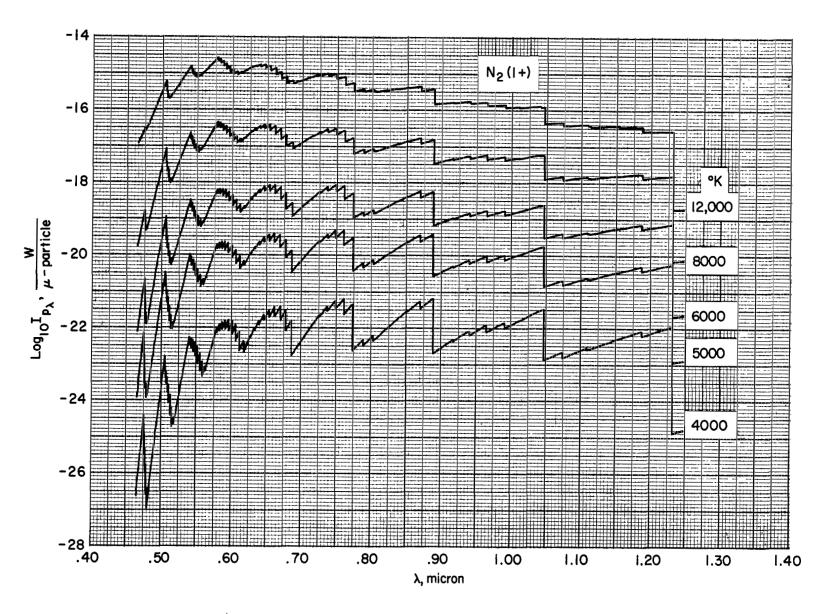


Figure 14.- Spectral intensity per particle for $N_2(1+)$ band system.

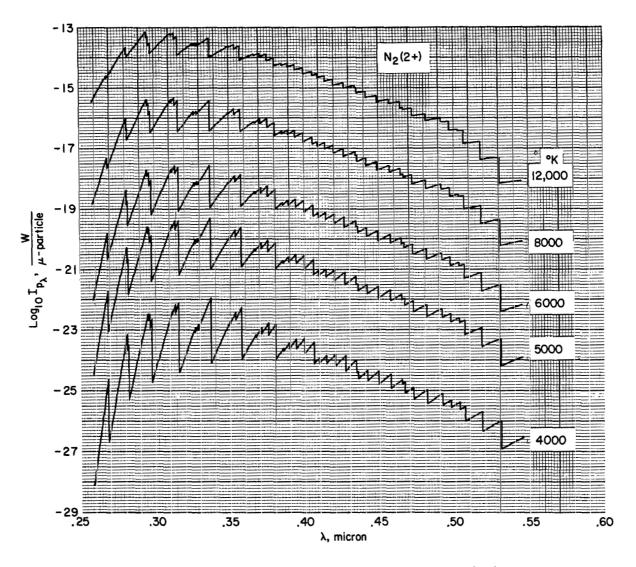


Figure 15.- Spectral intensity per particle for $N_2(2+)$ band system.

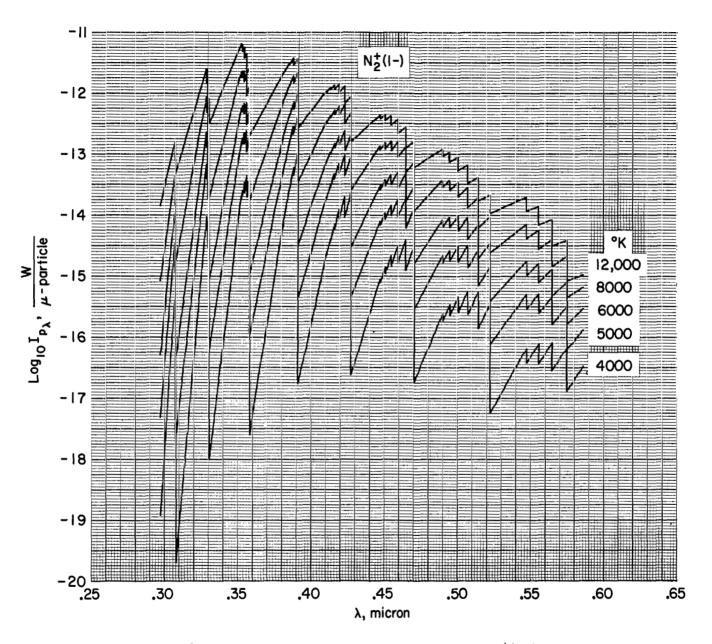


Figure 16.- Spectral intensity per particle for $N_2^+(1-)$ band system.

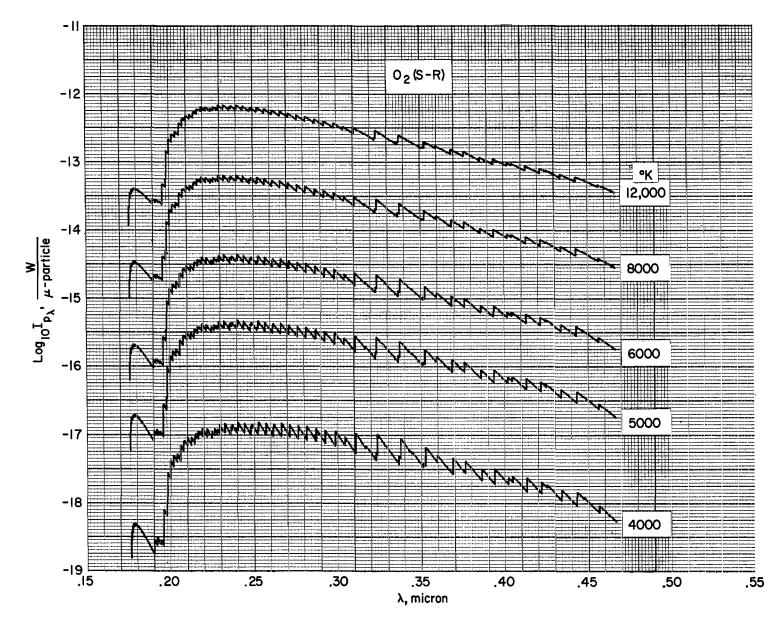


Figure 17.- Spectral intensity per particle for ${\rm O_2(S-R)}$ band system.

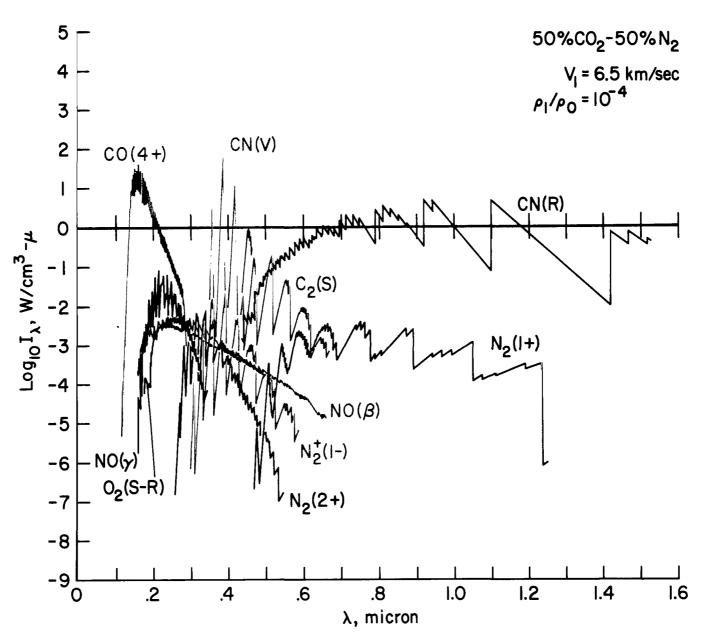


Figure 18.- Spectral intensity at $V_1 = 6.5$ km/sec and $\rho_1/\rho_0 = 10^{-4}$.

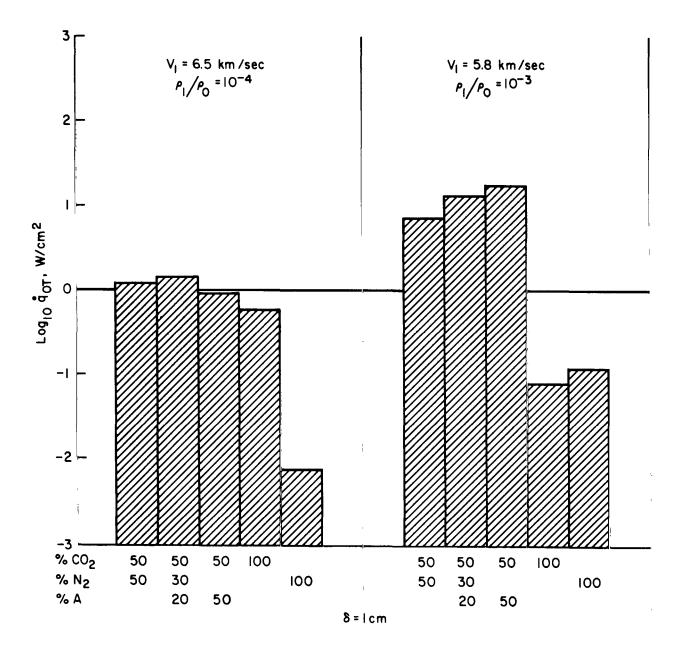


Figure 19.- Comparison of total heat-transfer rate in different gas mixtures.



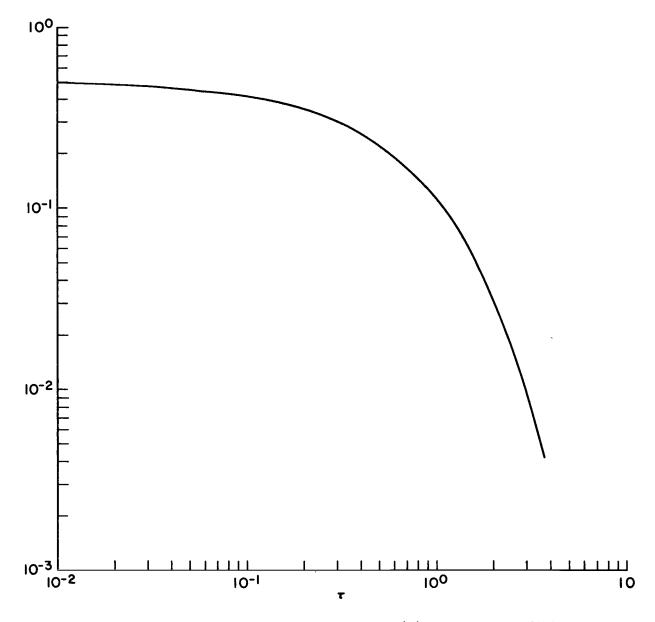


Figure 20.- Values of the function $E_3(\tau)$ in equation (12).

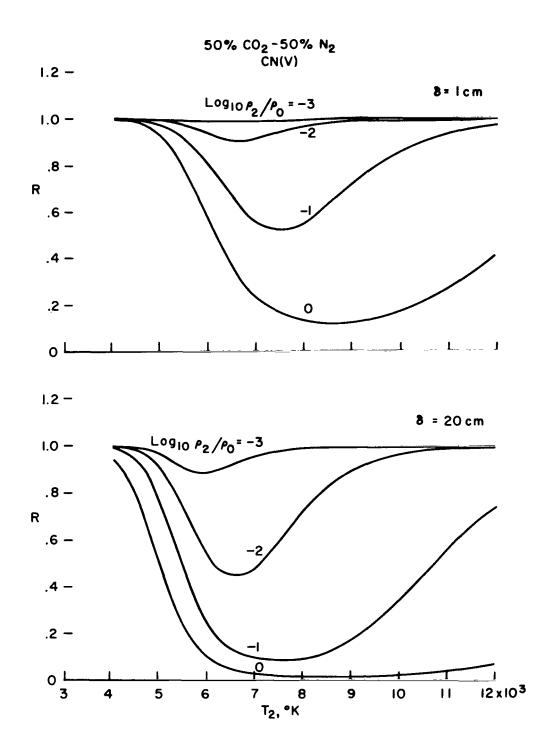


Figure 21.- Effect of self-absorption for CN violet band system.

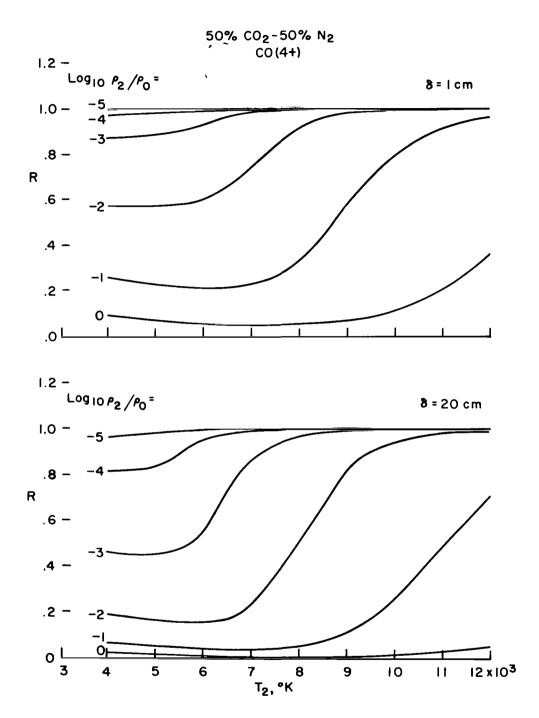


Figure 22.- Effect of self-absorption for CO fourth positive band system.

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